

## Correction of Serie 9 on the denormalization in frequency and in impedance

### Exercise 1

We choose the following topology of the 3<sup>rd</sup> order low-pass filter:

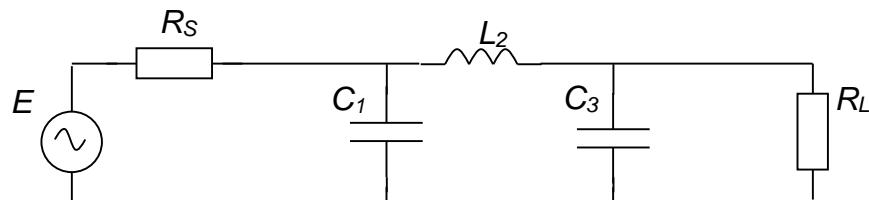


Fig. 1

The components were calculated in Serie 8 for which it is recalled that:

$R_s = 1$  Ohm and the specifications of Fig. 2 are fulfilled with  $A_3 = 1$  dB and  $A_1 = 30$  dB:

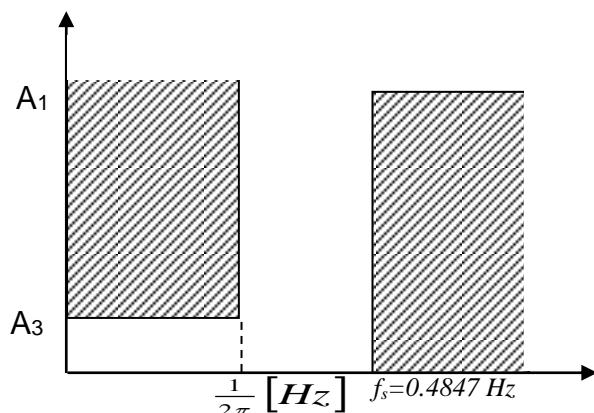


Fig. 2

# HF&VHF Circuits and Techniques I

The parameters are first calculated:

$$10 \log (1 + \varepsilon^2) = 1 \text{ dB}$$

which implies that

$$\varepsilon = 0.50885$$

$$h = \left( \frac{1}{\varepsilon} + \sqrt{1 + \frac{1}{\varepsilon^2}} \right)^{1/N} = \left( \frac{1}{0.50885} + \sqrt{1 + \frac{1}{0.50885^2}} \right)^{1/3} \approx 1.60961$$

$$\xi = h - \frac{1}{h} = 1.60961 - \frac{1}{1.60961} \approx 0.9883$$

The values of the components of Fig. 1, which fulfill the specifications of Fig. 2, are summarized below:

$$C_1 = \frac{4 \sin(\frac{\pi}{6})}{\xi R_s} = 2.023593 F$$

$$L_2 = \frac{1}{C_1} \cdot \frac{16 \sin(\frac{\pi}{6}) \sin(\frac{3\pi}{6})}{\xi^2 + [2 \sin(\frac{\pi}{3})]^2} = 0.994102 H$$

$$C_3 = \frac{1}{L_2} \cdot \frac{16 \sin(\frac{3\pi}{6}) \cdot \sin(\frac{5\pi}{6})}{\xi^2 + [2 \sin(\frac{2\pi}{3})]^2} = 2.023593 F$$

$$R_L = 1 \text{ Ohm}$$

## Denormalization in frequency and in impedance:

By comparing the specifications represented in Fig. 2 with respect to the new specifications represented in Fig. 3, we see that the end of the band-pass and the beginning of the stop-band have been multiplied by the same factor equal to:

$$10'000 / (1/2 \pi) = 2 \pi 10'000$$

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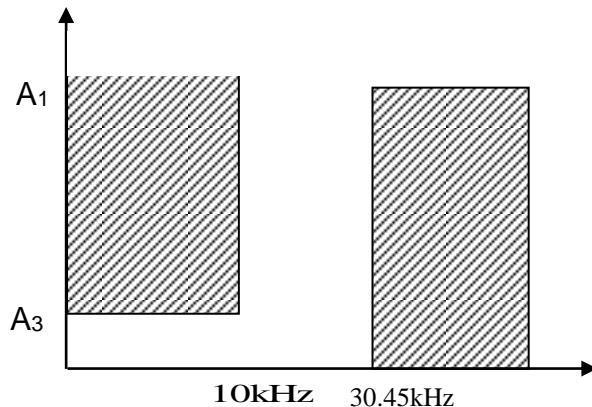
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# HF&VHF Circuits and Techniques I



**Fig. 3**

Moreover, the resistor of the source has been multiplied by 600.

Therefore, to fulfill the specifications of Fig. 3 with the assumption that  $R_s = 600$  Ohms:

- The two capacitors are divided by  $(2 \pi 10'000 \times 600) = 12'000'000 \pi$
- The inductor is divided by  $(2 \pi 10'000 / 600) = 33.3333 \pi$
- The resistor of the load is multiplied by 600

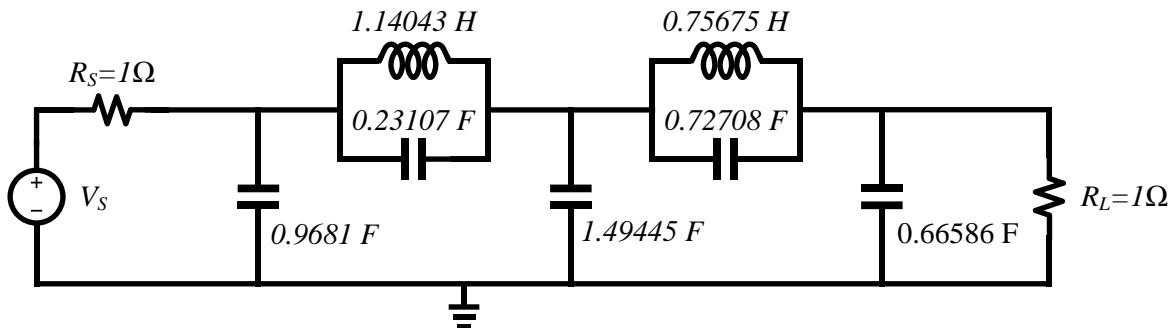
The below new values are obtained for the specifications of Fig. 3:

- $C_1 = C_3 = 53.6774715 \text{ nF}$
- $L_2 = 9.49297493 \text{ mH}$
- $R_L = 600 \text{ Ohms}$

# HF&VHF Circuits and Techniques I

## Exercise 2

The topology of a passive filter is given below:



**Fig. 1**

- $R_S = 1 \Omega$
- $C_1 = 0.9681 \text{ F}$
- $C_2 = 0.23107 \text{ F}, L_3 = 1.14043 \text{ H}$
- $C_4 = 1.49445 \text{ F}$
- $C_5 = 0.72708 \text{ F}, L_6 = 0.75675 \text{ H}$
- $C_7 = 0.66586 \text{ F}$
- $R_L = 1 \Omega$

**a) What is the type of this filter? Thanks to justify your answer.**

- In DC ( $f = 0 \text{ Hz}$ ), the capacitors corresponds to an open circuit and the inductors to a short circuit. Therefore, active power is delivered to the load  $R_L$ . In addition,  $R_S = R_L$ . Therefore, the maximum of power is delivered to the load in DC.
- At a very high frequency, the capacitors correspond to a short circuit and the inductors to an open circuit. Therefore, no active power is delivered to the load  $R_L$ .

**The two above properties prove that this filter is a low-pass filter.**

**b) Determine and calculate the frequencies for which the attenuation is very high**

- Each resonant circuit of the filter represented in Fig. 1 can be replaced by an open circuit at its resonant frequency.
- Therefore, at this resonant frequency, the attenuation is very high.

- The components of each resonant circuit and its corresponding resonant frequency are linked by:  $4\pi^2 f_0^2 = 1/(LC)$
- Therefore, we have two resonant frequencies which are equal to:  $f_1 = 0.21462004 \text{ Hz}$ ,  $f_2 = 0.3100374 \text{ Hz}$
- Moreover, at a very high frequency, the capacitors correspond to a short circuit and the inductors to an open circuit. Therefore, the attenuation is very high at a very high frequency.

**In summary, we have three poles of attenuation in:**

$f_1 = 0.21462004 \text{ Hz}$ ,  $f_2 = 0.3100374 \text{ Hz}$ ,  $f_3 = \text{infinity}$ .

c) It can be shown that the circuit of Fig. 1 fulfills the specifications of the attenuation represented in Fig. 2.

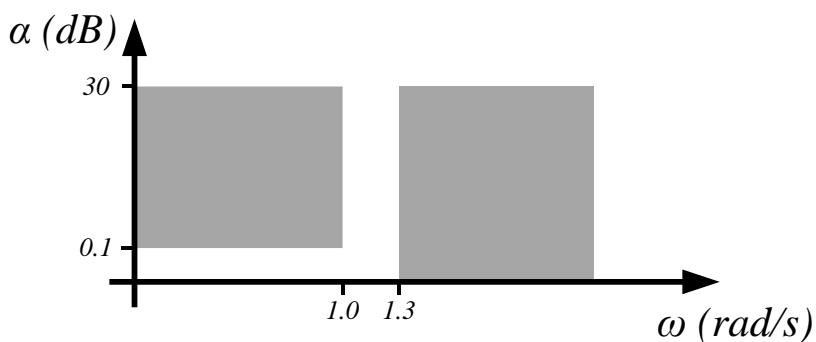


Fig. 2

**Calculate the values of the components of the new filter such that:**

**$R_s = R_L = 50 \text{ Ohms}$  and its cut-off frequency = 20 MHz.**

To fulfill these new specifications:

- the capacitors are divided by  $(2\pi \times 20 \times 10^6 \times 50) = 2 \times 10^9 \pi$
- the inductors are divided by  $(2\pi \times 20 \times 10^6 / 50) = 0.8 \times 10^6 \pi$
- the resistor of the load is multiplied by 50

Therefore, by starting from the voltage source generator, we obtain the following values of the components:

- $R_{s0} = 50 \text{ Ohm}$
- $C_{10} = 0.154078 \text{ nF}$
- $C_{20} = 0.0367759 \text{ nF}$ ,  $L_{30} = 0.453763 \text{ uH}$
- $C_{40} = 0.237849 \text{ nF}$
- $C_{50} = 0.115718 \text{ nF}$ ,  $L_{60} = 0.301101 \text{ uH}$

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- $C_{70} = 0.105975 \text{ nF}$
- $R_{L0} = 50 \text{ Ohm}$

## Determine and calculate the frequencies for which the attenuation is very high

In comparison to the question b), the frequencies of the three poles of attenuation are multiplied by  $2\pi \times 20 \times 10^6$  due to the denormalization in frequency. Therefore, we obtain:

$$f_{10} = 26.969950 \text{ MHz}, f_{20} = 38.960448 \text{ MHz}, f_{30} = \text{infinity}$$

### Remark:

The denormalization in impedance has no effect on the values of these frequencies because this denormalization does not affect the multiplication ( $L \times C$ ) for each resonant circuit.